

1. at Triode-sat boundary: FETs have $V_{os} = V_{gs} - V_{t}$

→ all FETs have current I !

→ M1: $I = \frac{1}{2} k \frac{w_1}{L_1} (V_{gs} - V_{t})^2 = \frac{1}{2} k \frac{w_1}{L_1} (V_{v1} - V_{t})^2$

→ M2: $I = \frac{1}{2} k \frac{w_2}{L_2} (V_{v2} - V_{v1} - V_{t})^2 = \frac{1}{2} k \frac{w_2}{L_2} (V_{v2} - (V_{v1} - V_{t}) - V_{t})^2$
 $= \frac{1}{2} k \frac{w_2}{L_2} (V_{v2} - V_{v1})^2$

→ M3: $I = \frac{1}{2} k \frac{w_3}{L_3} (V_{v2} - V_{t})^2$

→ all these currents are equal! $\therefore \frac{w_2}{L_2} \frac{I_{M3}}{(V_{v2} - V_{t})^2} = \frac{w_1}{L_1} \frac{I_{M2}}{(V_{v2} - V_{v1})^2} = \frac{w_1}{L_1} \frac{I_{M1}}{(V_{v1} - V_{t})^2}$

$V_{v2} - V_{v1} = V_{v1} - V_{t}$

$V_{v2} = 2V_{v1} - V_{t}$

$\frac{w_2}{L_2} (2V_{v1} - V_{t} - V_{t})^2 = \frac{w_1}{L_1} (V_{v1} - V_{t})^2$

$4 \frac{w_2}{L_2} = \frac{w_1}{L_1}$

2. a) $V_y = V_x$ implies M2 is in sat mode

equating $I_{M1}, I_{M2} \dots$ you always have as many expressions/equations as you have FETs!

$\frac{1}{2} k \frac{w}{L} (V_{cc} - V_x - V_{t})^2 = \frac{1}{2} k \frac{w}{L} (V_x - V_{t})^2$

$(6 - V_x)^2 = (V_x - 2)^2$

~~$V_x^2 - 8V_x + 32 = 0$~~ $\rightarrow V_x = 4$

→ we could have also found this using symmetry

b) now M2 is in triode

$\frac{1}{2} k \frac{w}{L} (6 - V_x)^2 = k \frac{w}{L} \left[(V_x + 3 - V_{t}) V_x - \frac{1}{2} V_x^2 \right]$

$V_x^2 - 12V_x + 36 = 2 \left[\frac{1}{2} V_x^2 + 3V_x - 2V_x \right] \rightarrow -12V_x + 36 = V_x$

$V_x = \frac{36}{13} = 3$

c) New $V_{cc} \dots V_x=3, V_y=6, I=2\text{mA}$

\rightarrow can't work with M1 (don't know V_{cc} !)

\rightarrow make easier: $I=2\text{mA} = k'_n \frac{W}{L} \left[(6-2)3 - \frac{1}{2}(3)^2 \right]$

$$= \left[12 - \frac{9}{2} \right] \cdot k'_n \frac{W}{L}$$

$$k'_n \frac{W}{L} = 2\text{mA} \left[12 - \frac{9}{2} \right]^{-1} = \boxed{.27 \text{ mA/V}^2}$$

3. For the 1st circuit:

$$I_1 = \frac{1}{2} k'_n \frac{W}{L} [V_2 - 1]^2 = \frac{1}{2} k'_n \frac{W}{L} [3 - 1]^2$$

$$V_2^2 - 2V_2 + 1 = 4 - 4V_2 + V_2^2$$

$$2V_2 = 3$$

$$V_2 = 1.5 \text{ V}$$

$$I_1 = \frac{1}{2} (20\mu)(3) [1.5 - 1]^2$$

$$= 20\mu \frac{3}{8} = 7.5 \mu\text{A}$$

~~For the 2nd circuit~~

recall V_G negative!

We have: $I_3 = \frac{1}{2} k'_p \frac{W}{L} [V_4 - 3 + 1]^2 = \frac{1}{2} k'_p \frac{W}{L} [V_4 - 1]^2$

$$k'_p [V_4^2 - 4V_4 + 4] = 2.5 k'_p [V_4^2 - 2V_4 + 1]$$

$$1.5V_4^2 - V_4 - 1.5 = 0$$

$$V_4^2 - \frac{V_4}{1.5} - 1 = 0 \rightarrow \frac{\frac{2}{3} \pm \sqrt{\frac{4}{9} + 4}}{2}$$

check that $V_{GS} > V_G \dots$ o/c

$$I = \frac{1}{2} (20\mu)(3) [1.387 - 1]^2 = 4.5 \mu\text{A}$$

4. Since $V_{GS} = 5V$, $V_{DS} < 5V$... probably in Triode ($V_{DS} \leq V_{GS} - 1$)

Let us set $V_{DS} = 50mV$ (small V_{DS} ! can use $r_{DS} \approx \frac{1}{k \frac{w}{L} (V_{GS} - V_T)}$)

$$50\Omega \approx \frac{1}{100\mu \left(\frac{w}{L}\right) (5-1)} \Rightarrow \text{solve } \boxed{\frac{w}{L} = 50}$$

$$V_{DS} = 50mV \rightarrow \frac{V_{DD} - V_{DS}}{R} = I = k \frac{w}{L} \left[(5-1)50m - \frac{1}{2}50m^2 \right]$$

$$R = \frac{5 - 50m}{100\mu(50) \left[200m - \frac{1}{2}(2.5m) \right]} = \boxed{4.981 k\Omega}$$

Also

Brief derivation of g_m for a FET amplifier

$$i_D = \frac{1}{2} k \frac{w}{L} (v_{GS} - V_T)^2 ; v_{DS} = V_{DD} - R_D i_D$$

$$\therefore v_{DS} = V_{DD} - \frac{1}{2} R_D k \frac{w}{L} (v_{GS} - V_T)^2$$

$$A_v = \left. \frac{\partial v_{DS}}{\partial v_{GS}} \right|_{v_{GS} = V_{GSQ} \text{ (at some bias point } Q)}$$

$$= -R_D k \frac{w}{L} (V_{GSQ} - V_T) = -R_D g_m \text{ where } g_m \equiv k \frac{w}{L} (V_{GSQ} - V_T)$$