



Outline of Section 3 - Diodes

- Two terminal devices
- Diode models
- Exponential model
- Constant voltage drop model
- Reverse breakdown
- Applications
- Small-signal model
- PN junctions



Rectification

- Essential building block of AC to DC conversion
- Makes AC input unipolar at output
- Imposes average DC value on output

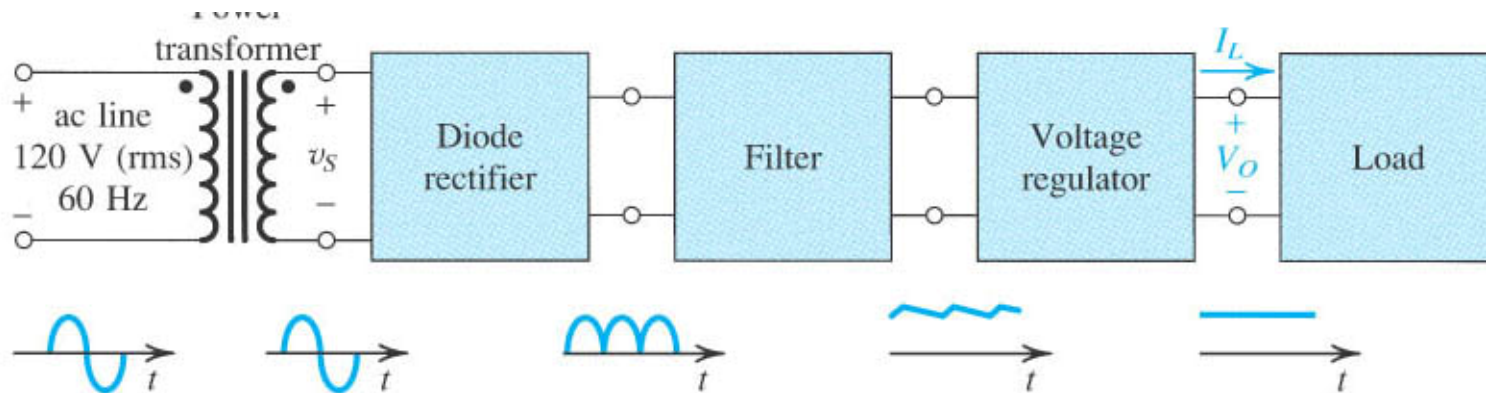


Figure 3.24 Block diagram of a dc power supply.



Rectification – Operation

Let $v_S(t)$ be a sine wave

$$v_S(t) = V_{DC} + V_p \sin(\omega t)$$

For positive v_S :

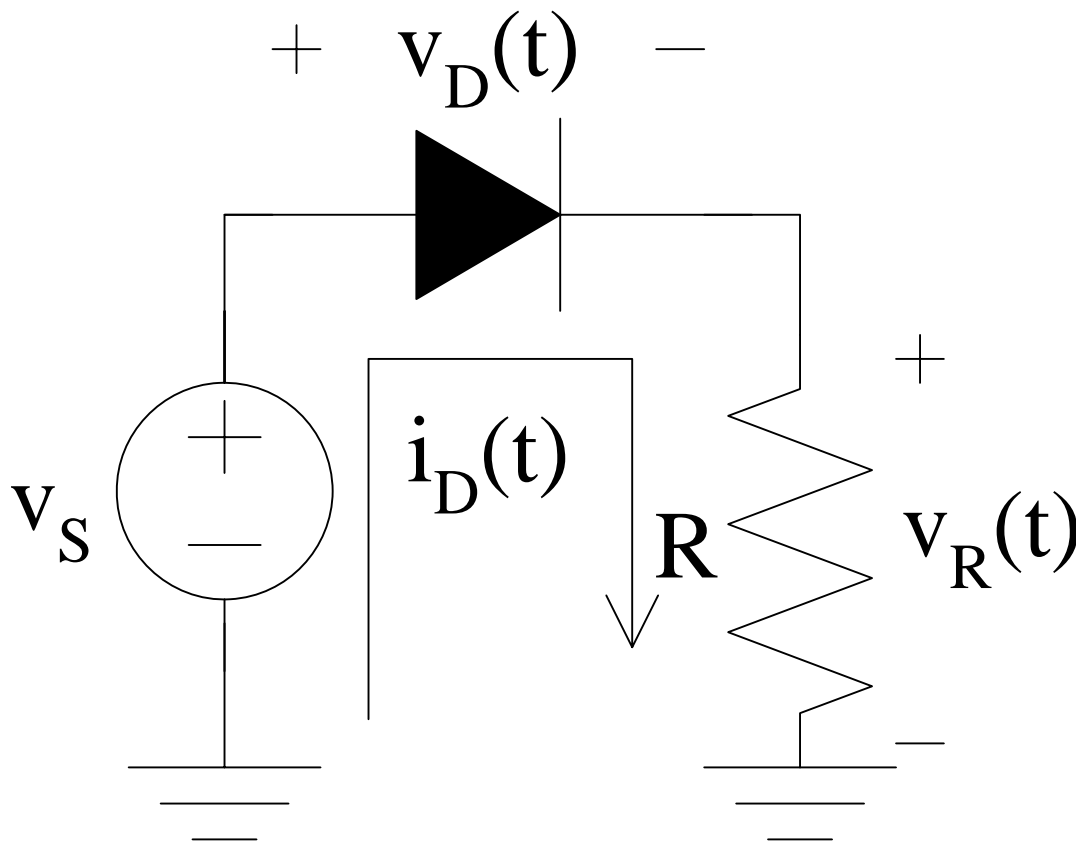
$$i_D = 0 \text{ for } v_S \leq 0.7V$$

When diode conducts:

$$v_R(t) = v_S(t) - 0.7$$

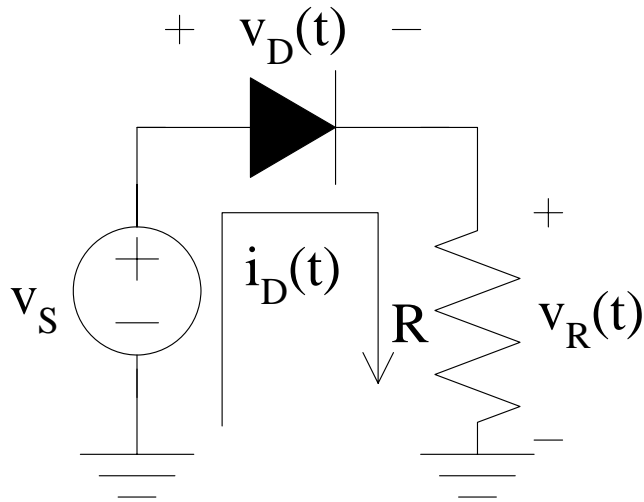
For negative v_S :

$$i_D = 0, v_R = 0, \\ v_D(t) = v_S(t)$$





Half-Wave Rectifier



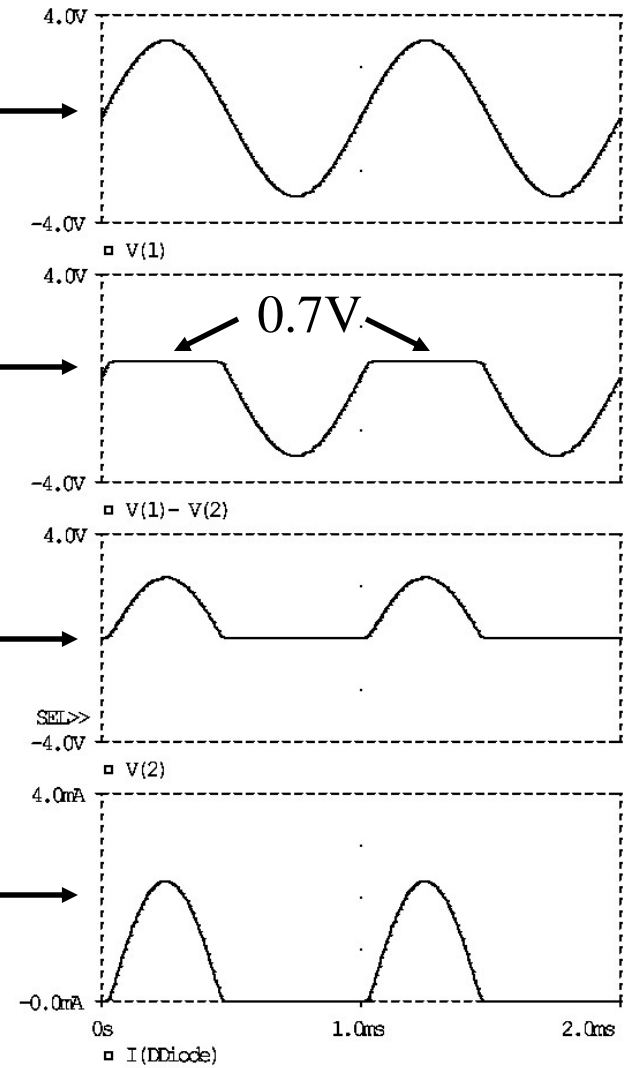
Signal source

Voltage drop across diode with CVDM

Voltage across resistor

- rectified signal
- v_S minus diode drop

Circuit current flow





Fullwave Rectifier

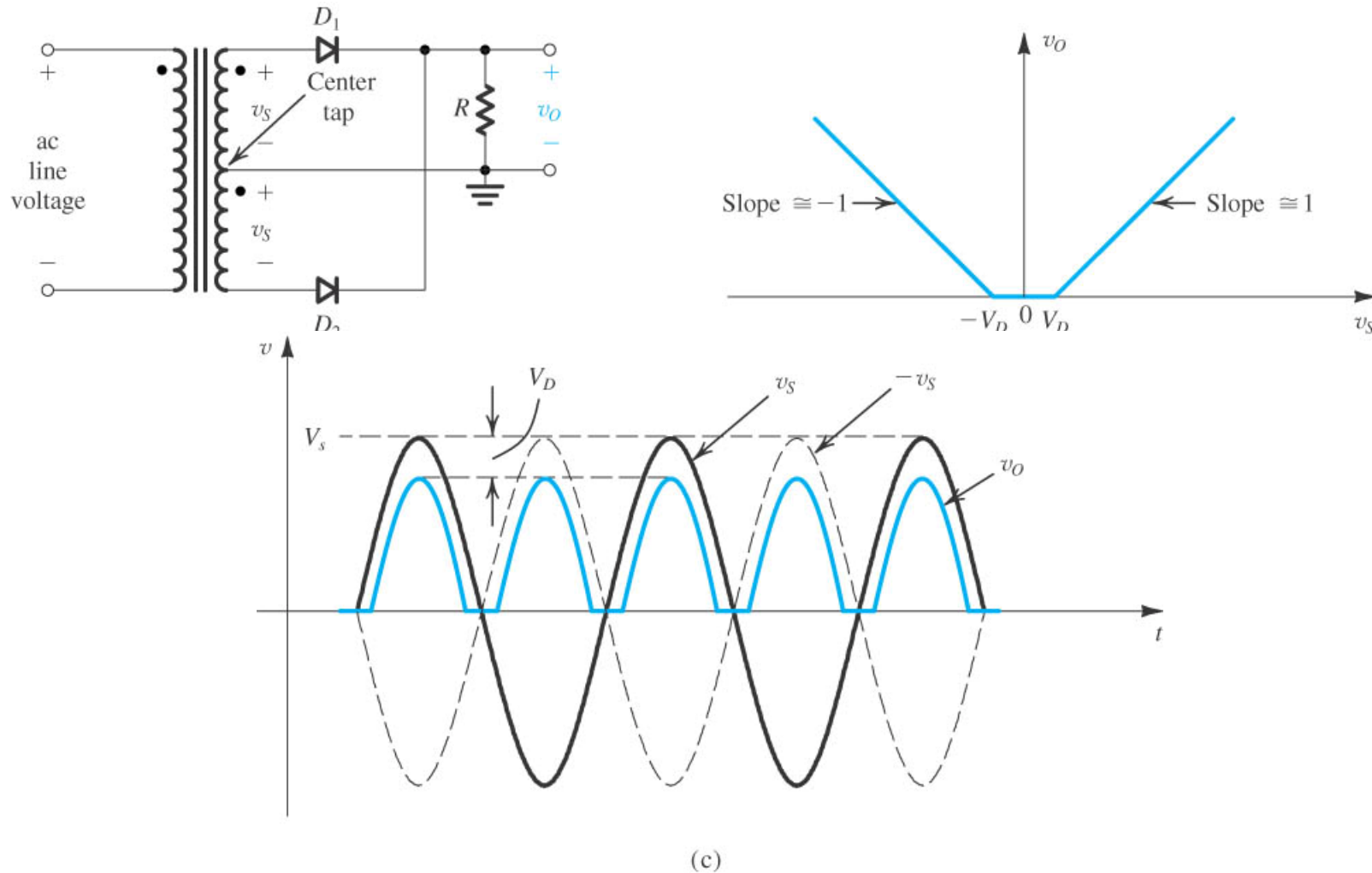
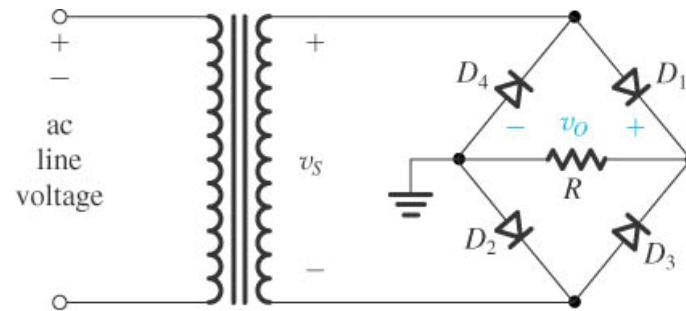


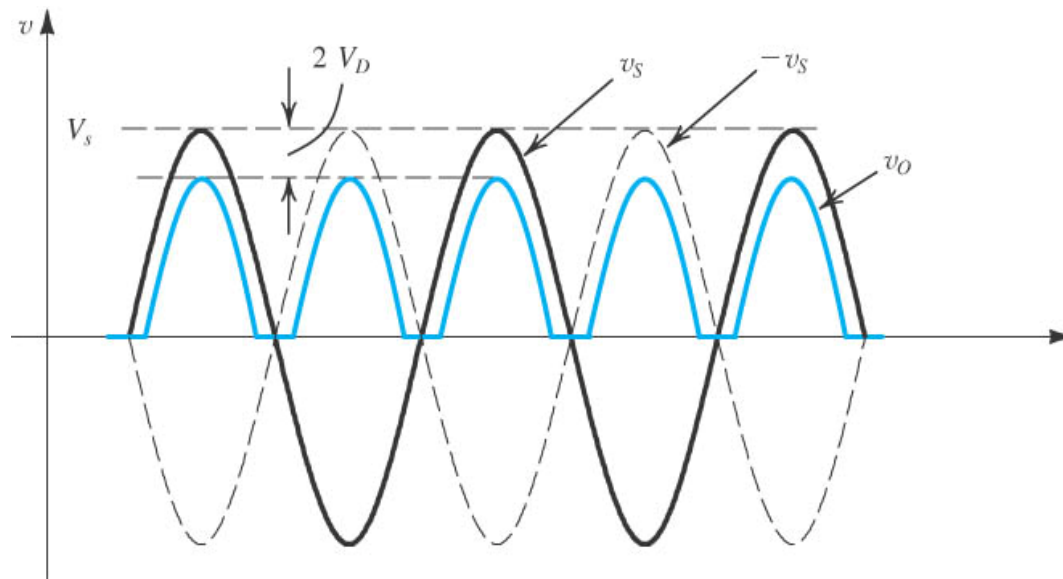
Figure 3.26 Full-wave rectifier utilizing a transformer with a center-tapped secondary winding: (a) circuit; (b) transfer characteristic assuming a constant-voltage-drop model for the diodes; (c) input and output waveforms.



Bridge Rectifier



(a)



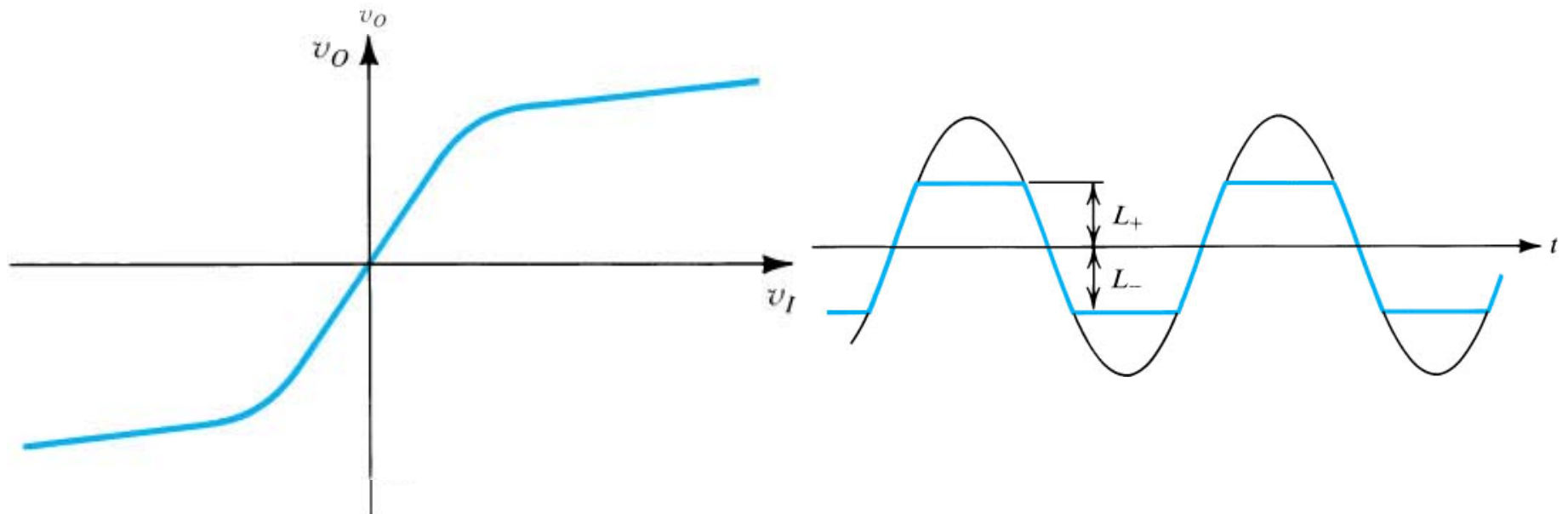
(b)

Figure 3.27 The bridge rectifier: (a) circuit; (b) input and output waveforms.



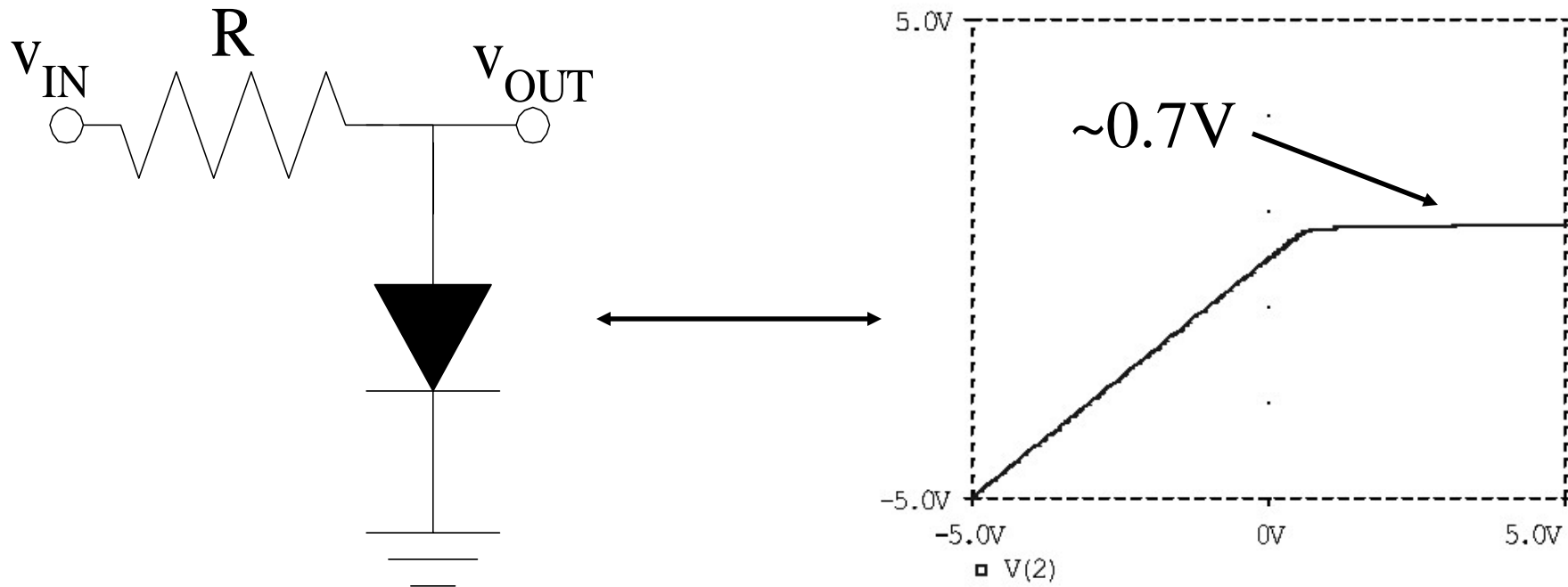
Limiting Circuits – Purpose

- Limiting circuits prevent output signals from exceeding and/or going below certain voltages
- Used for over and undershoot protection at the inputs of logic gates
- Used to perform waveform-shaping functions





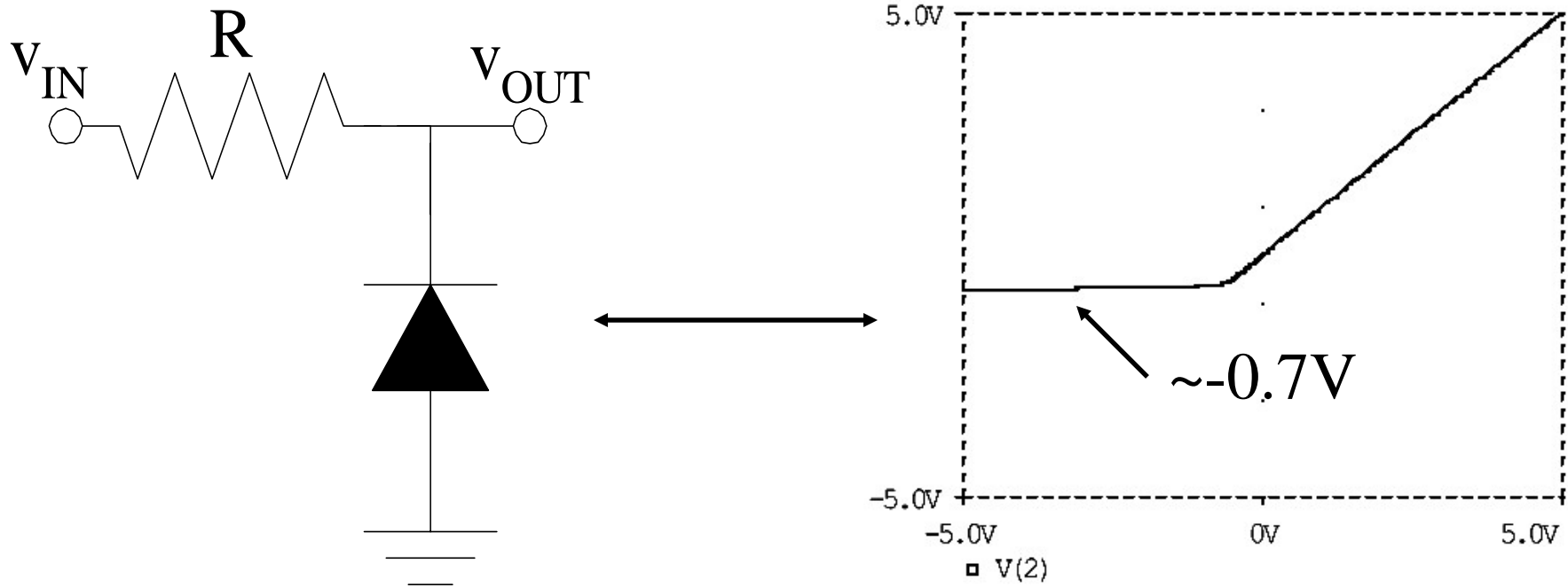
Overshoot Limiter



- If V_{IN} gets too large, diode conducts and clamps V_{OUT} to approximately a diode drop above ground
- Slope of transition region = 1 because no load attached thus no current drawn through resistor



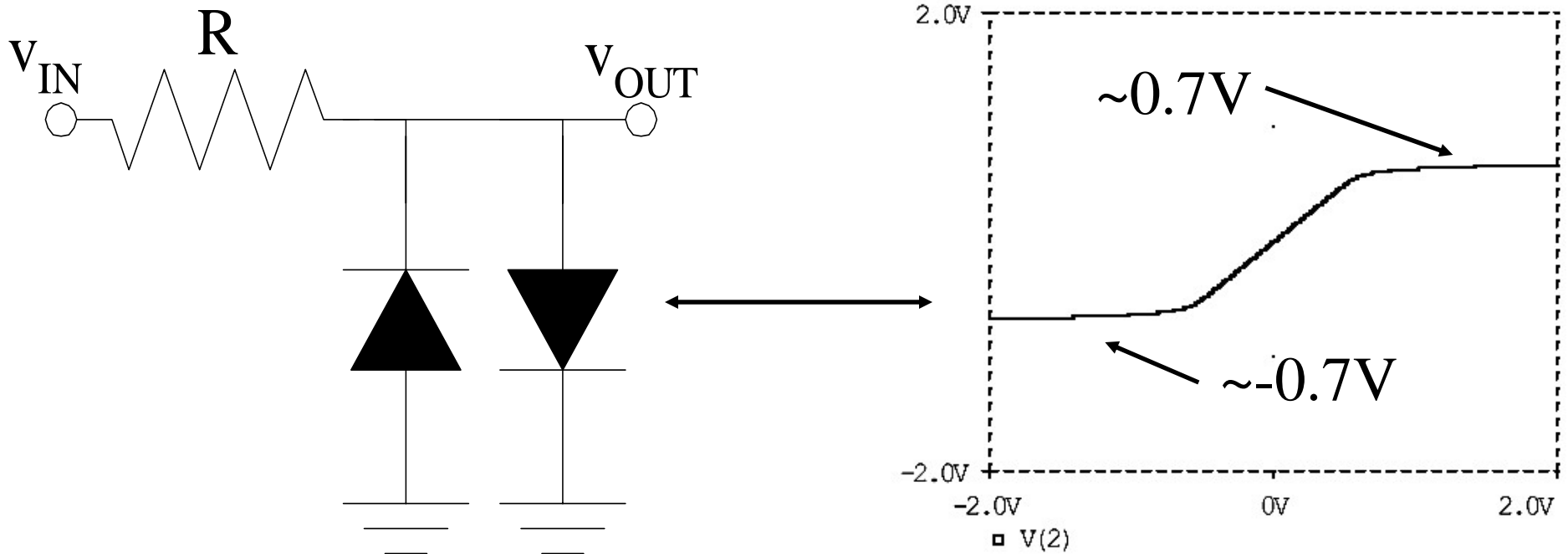
Undershoot Limiter



- If V_{IN} gets too negative, diode conducts and clamps V_{OUT} to approximately a diode drop below ground



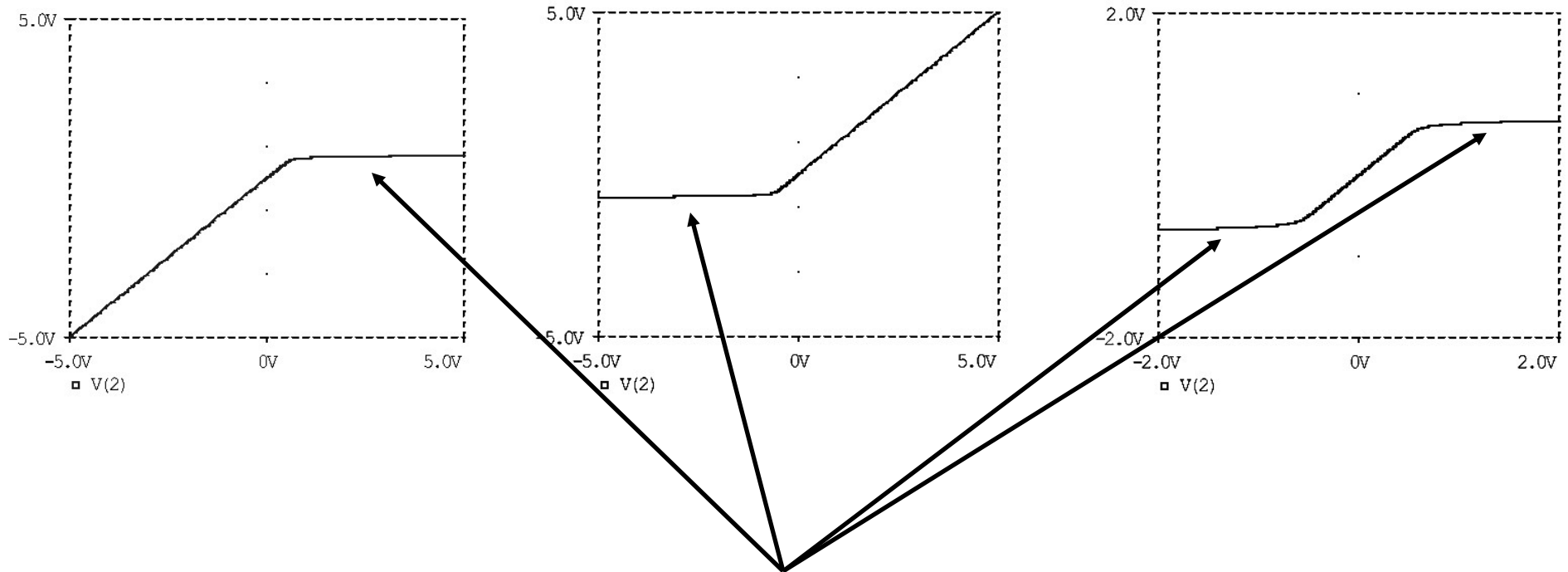
Double Limiter



- If V_{IN} gets too positive or negative, a diode conducts to clamp V_{OUT} to approximately a diode drop above or below ground



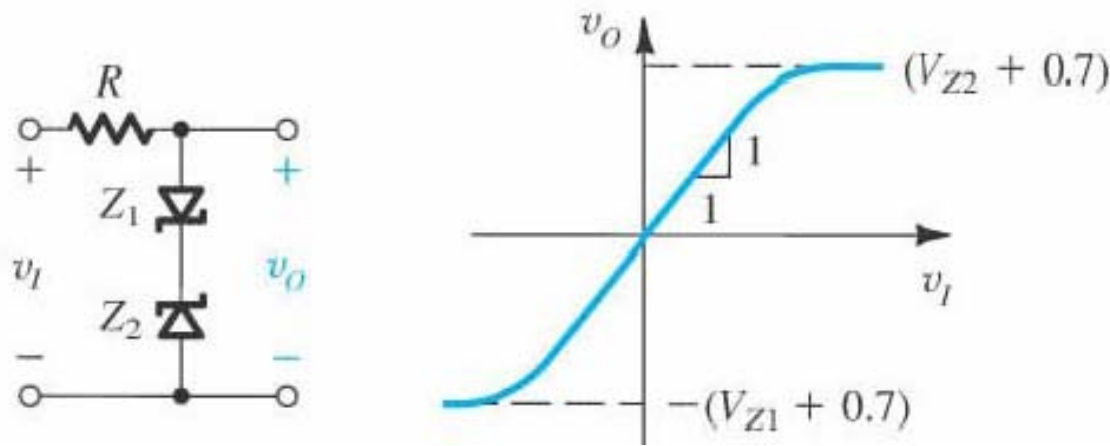
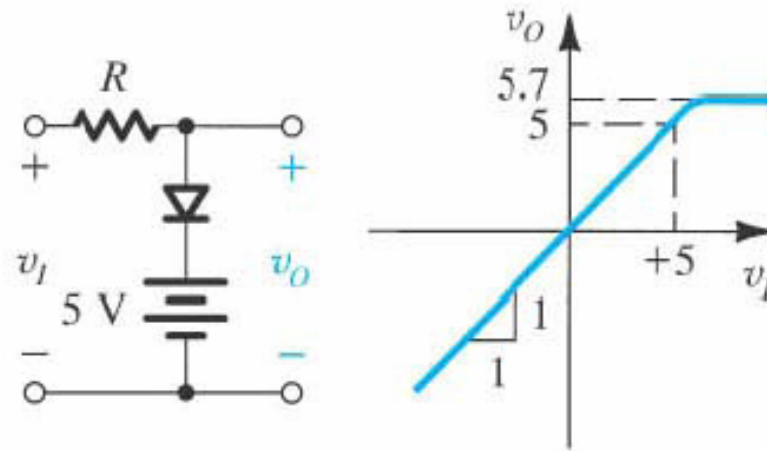
VTCs



- “Flat” portions of VTC’s have small but finite slope due to ‘on-resistance’ of diode
- Slope of transition regions = 1 because no load attached thus no current drawn through resistor



Other Limiting Circuits



**Double-anode
Zener**

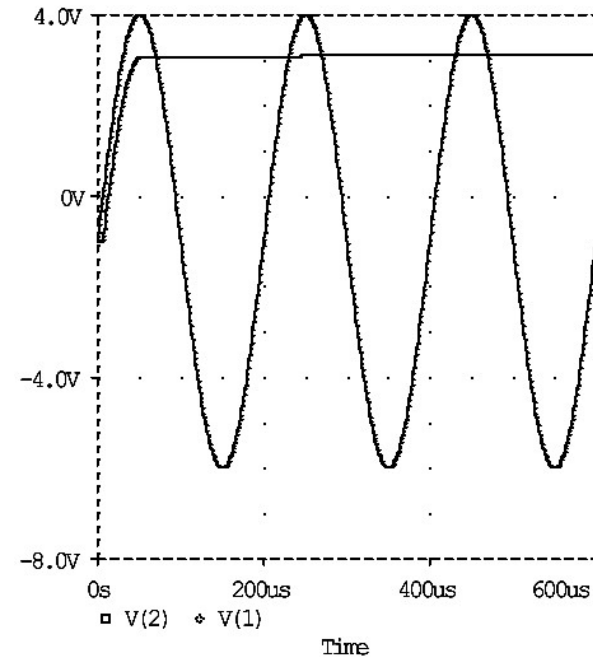
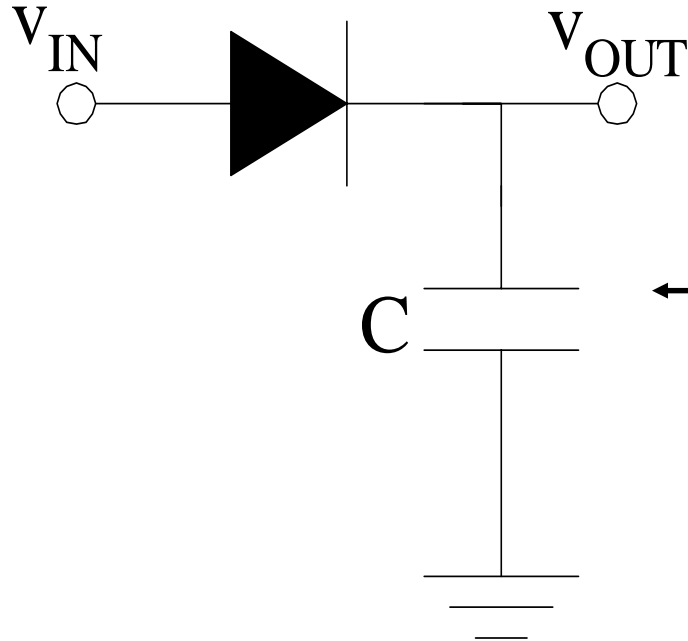


Clamping Circuits – Purpose

- Detect peak signal levels
- Remove DC offsets or restore DC
- Voltage doubling (double peak-clamping)
- Construct AC to DC converters
- Receive amplitude modulated signals (e.g. radio)



Peak Detection



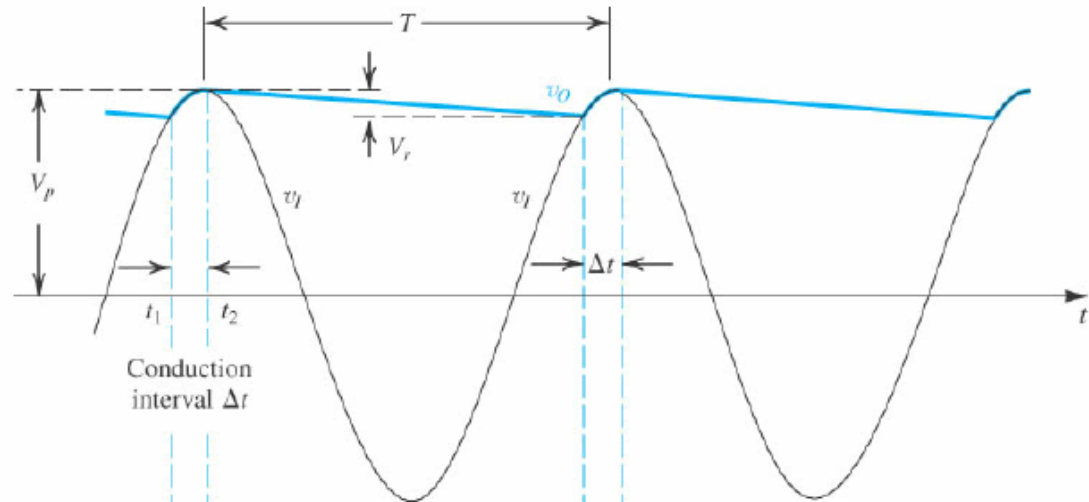
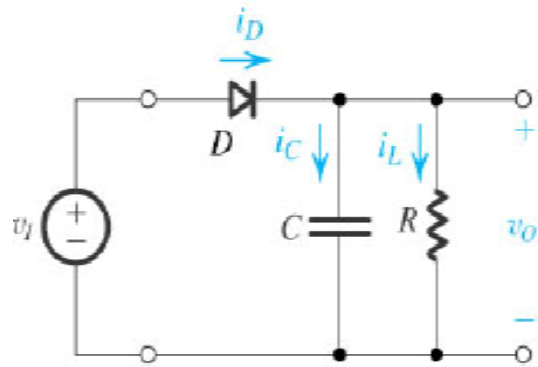
- This circuit is also known as a rectifier with a filter capacitor

Operation:

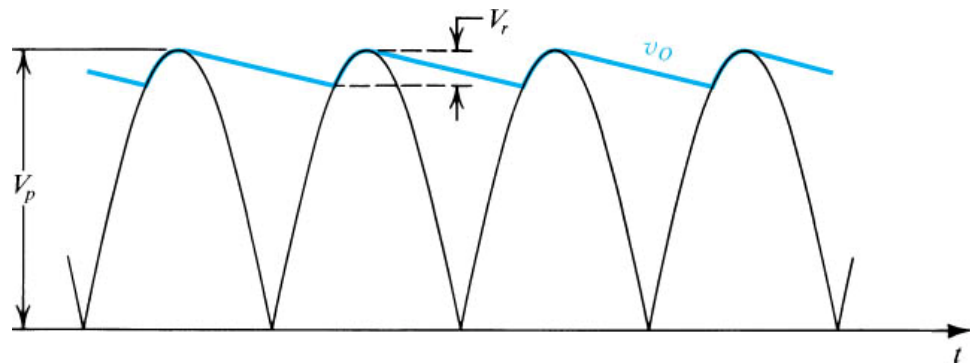
- charge is injected into capacitor whenever diode conducts
- circuit detects signal peak minus a diode drop
- current loss during reverse-bias neglected



Peak Detection



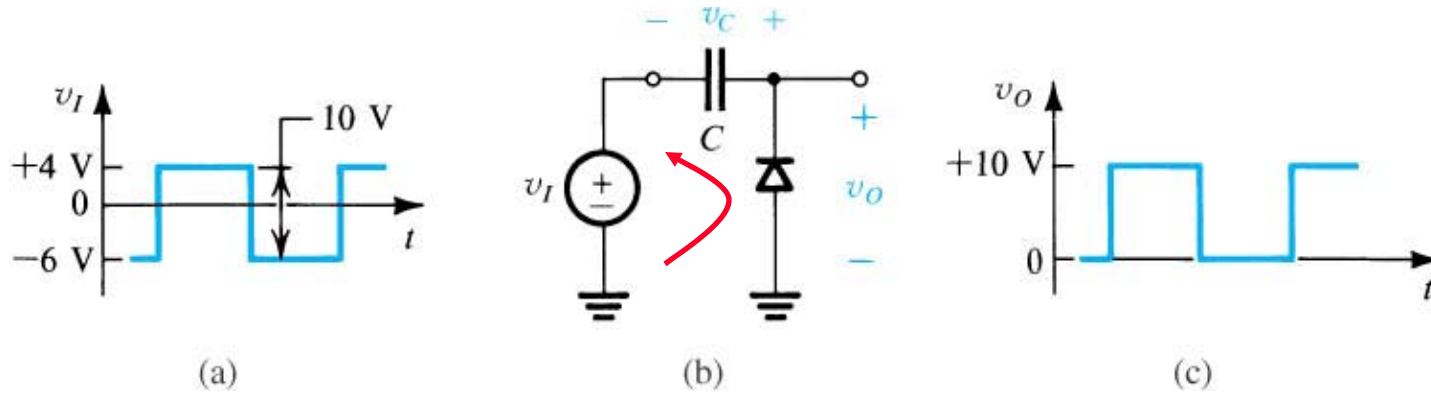
If we have a Fullwave Rectifier before peak detection



- Basis for **AM demodulators** and **AM receivers**
- You will see more about this (calculations of conduction time, ripple voltage, average and peak currents, etc.) **in EC2 lab**



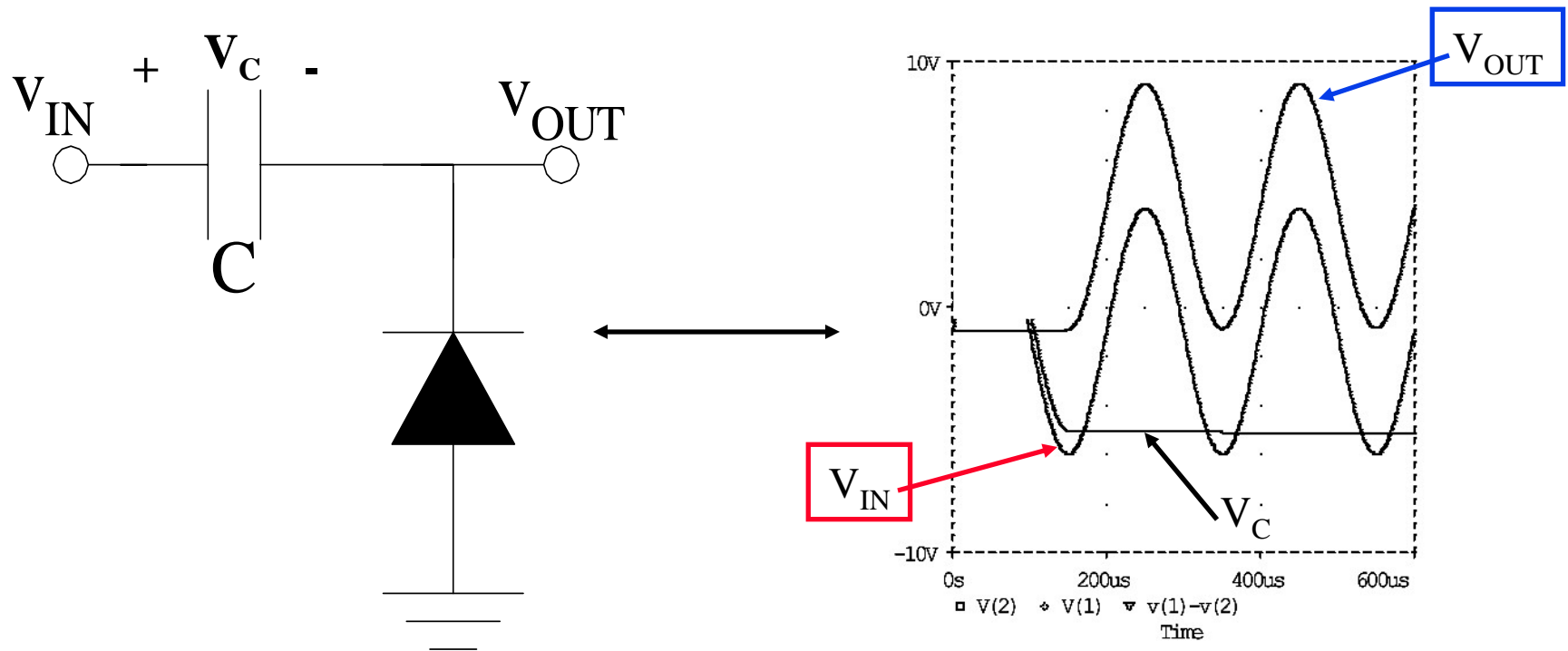
DC Restorer or Clamped Capacitor



- Operation considering Ideal Model for the diode:
 - At the beginning when $v_I = -6\text{V}$, the diode conducts and the capacitor charges up to 6 V, $v_C = 6\text{V}$
 - When $v_I = +4\text{V}$, the voltage drop across the diode is $v_I + v_C = v_O = 6 + 4 = 10\text{V}$, therefore the diode is off, no current goes through the diode and $v_O = v_I + v_C$
 - This is how a DC shift appears at the output



Another Example with CVDM



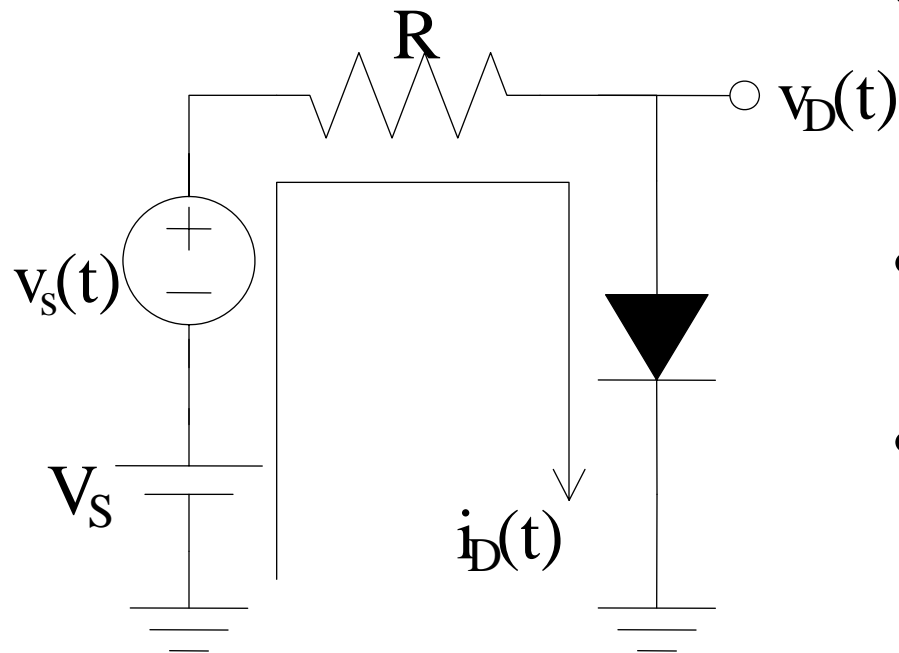
- as V_{IN} falls below $-0.7V$, capacitor charged by diode
- V_C clamps at a diode drop above the negative input peak
- diode prevents capacitor discharge, removing most of DC offset



Outline of Section 3 - Diodes

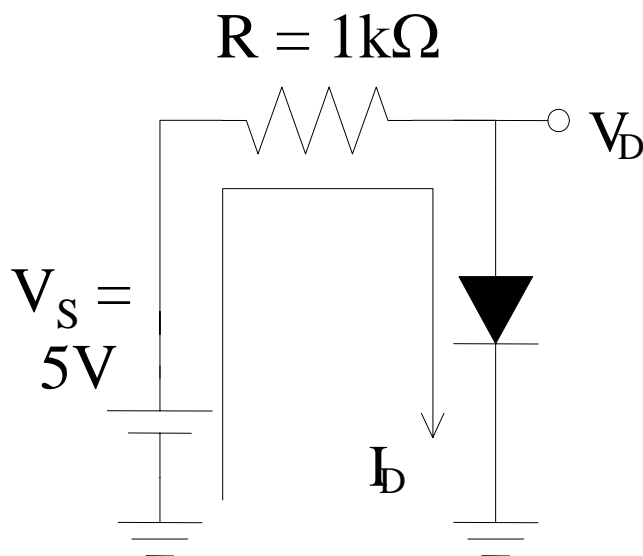
- Two terminal devices
- Diode models
- Exponential model
- Constant voltage drop model
- Reverse breakdown
- Applications
 - **Note:** Voltage Doubler and Super Diode applications and calculations of conduction time, ripple voltage, average and peak currents of peak rectifier circuit are not covered
- Small-signal model
- PN junctions

Mixed DC and AC Analysis



- Consider circuit contains DC and AC sources, resistors and diodes
- Linear superposition of the signals applies
- Therefore, we can separate our analysis into two sets:
 1. DC analysis
 2. AC analysis

DC analysis to determine the Operating Point



- 1) “Kill” AC sources
- 2) Perform DC analysis on the remaining DC circuit.
- 3) Make an assumption about the state of the diodes.
- 4) Use **Exponential or CVDM** to find the DC voltages and currents.

For example, in this circuit, if exponential model is used. we follow iterative solution or graphical solution:

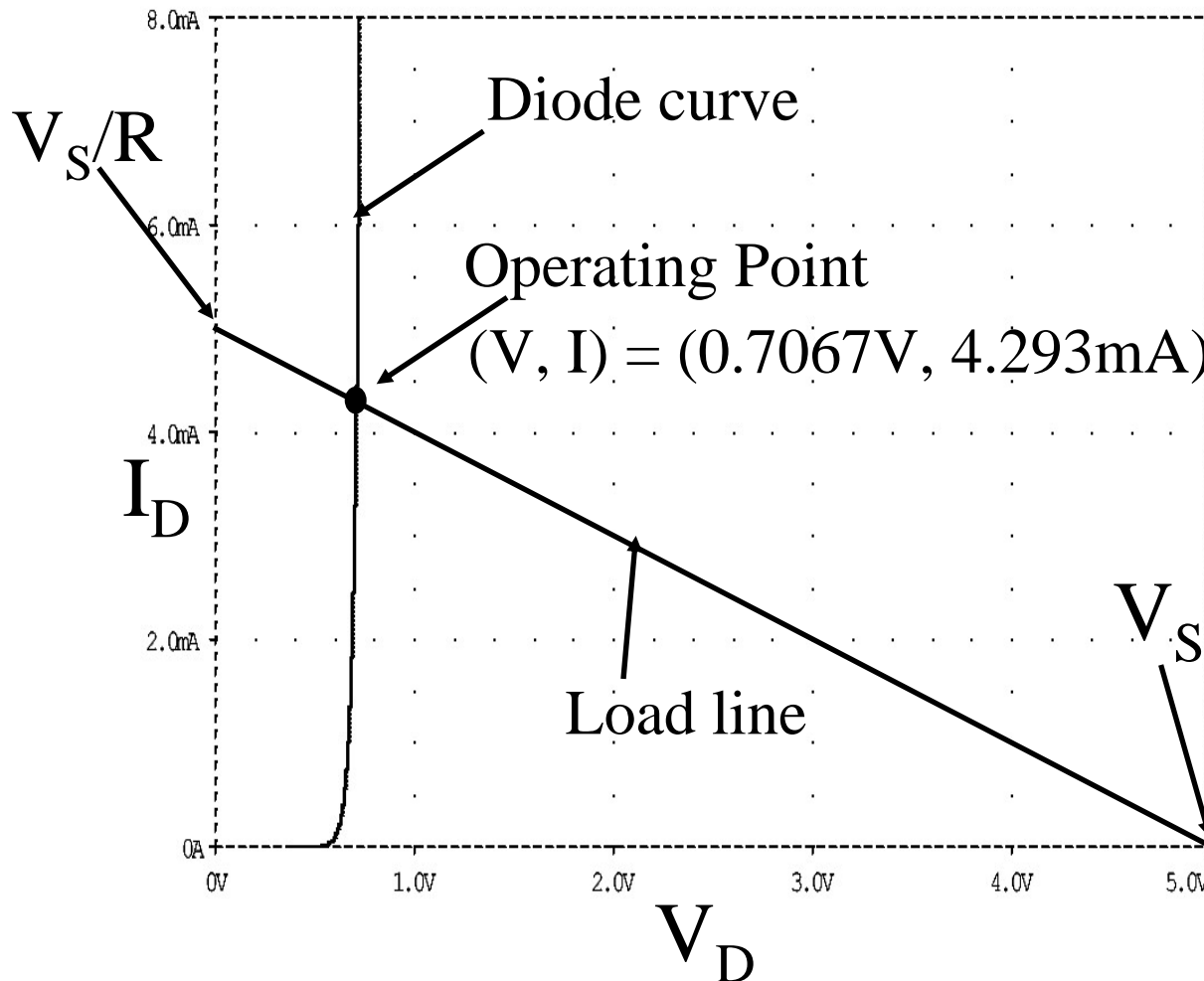
- a) Assume diode is in strong forward bias

and governed by:
$$I_D = I_S e^{V_D/nV_T}$$

- b) Kirchhoff loop equation:
$$I_D = \frac{V_S - V_D}{R}$$



Example: Graphical Analysis

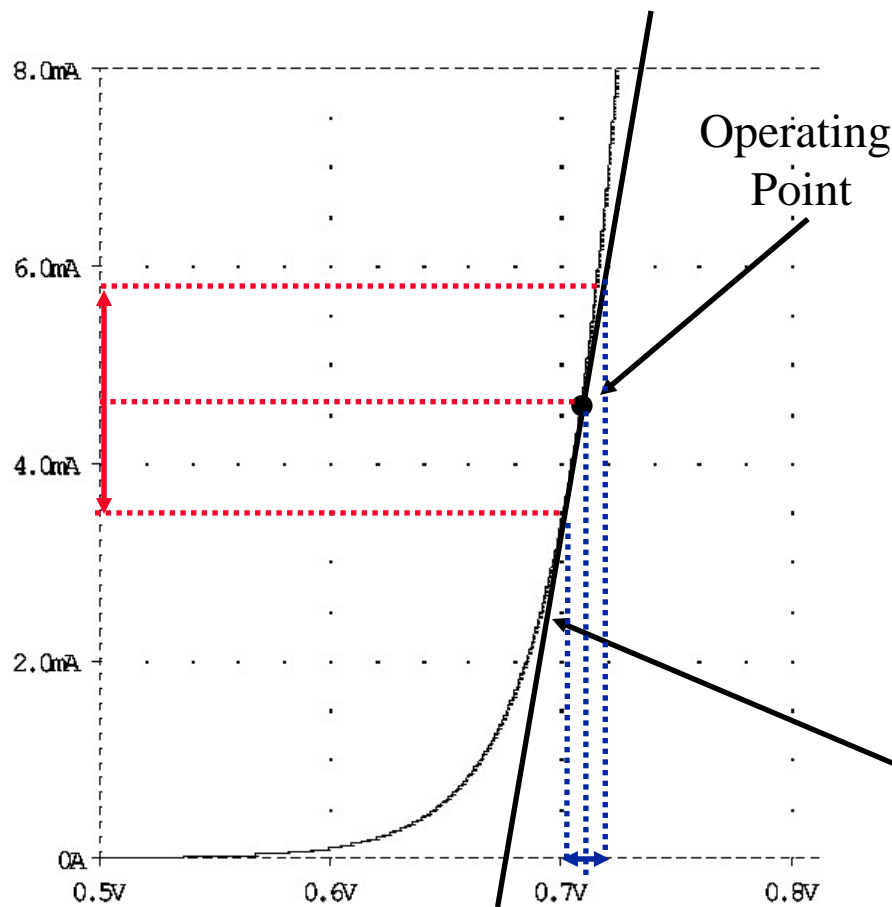


- 1) Plot two relationships on the i-v plane.
- 2) The solution is the intersection of the two graphs; operating point



AC Analysis: Diode Small Signal Model

Consider superposition of an AC signal at the DC operating point:



- a) A ΔV will result in a ΔI
- b) If ΔV is small, the resulting ΔI will be related linearly to ΔV
- c) *Slope* of I-V curve *at the operating point* is defined as *the diode small signal conductance/resistance*:

$$g_m \equiv \frac{1}{r_d} \equiv \left. \frac{\partial i_D}{\partial v_D} \right|_{OP} \approx \frac{\Delta I}{\Delta V}$$



Derivations to Find Diode's Small-Signal Resistance – r_d

To derive an expression for r_d , we use the exponential model and calculate the derivative at DC operating point:

$$\underline{\text{Define:}} \quad r_d \equiv \left[\frac{\partial i_D}{\partial v_D} \Big|_{OP} \right]^{-1} \quad i_D = I_S \left[e^{v_D/nV_T} - 1 \right]$$

$$\frac{\partial i_D}{\partial v_D} = I_S \exp\left(\frac{v_D}{n \cdot V_T}\right) \cdot \frac{1}{n \cdot V_T} \quad I_S \exp\left(\frac{v_D}{n \cdot V_T}\right) = i_D + I_S$$

$$\therefore \frac{\partial i_D}{\partial v_D} = \frac{i_D + I_S}{n \cdot V_T} \approx \frac{i_D}{n \cdot V_T}$$

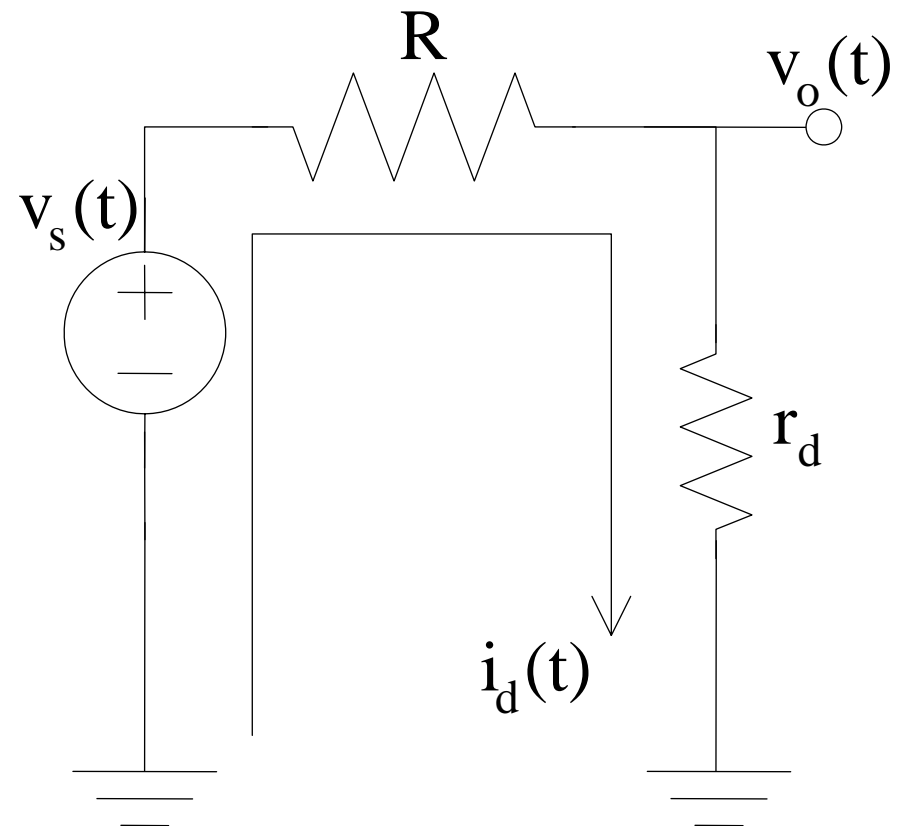
$$\boxed{r_d = \frac{n \cdot V_T}{I_D}}$$

Now plug in the operating point (the DC value of I_D) to find r_d



Complete AC Analysis

- The result of linearization around DC operating point is that **AC signals see the forward biased diode as a resistor: r_d**
- Based on this result, we construct **the small-signal equivalent circuit** as shown
- Perform circuit analysis – in this case it is just a voltage division to find v_o





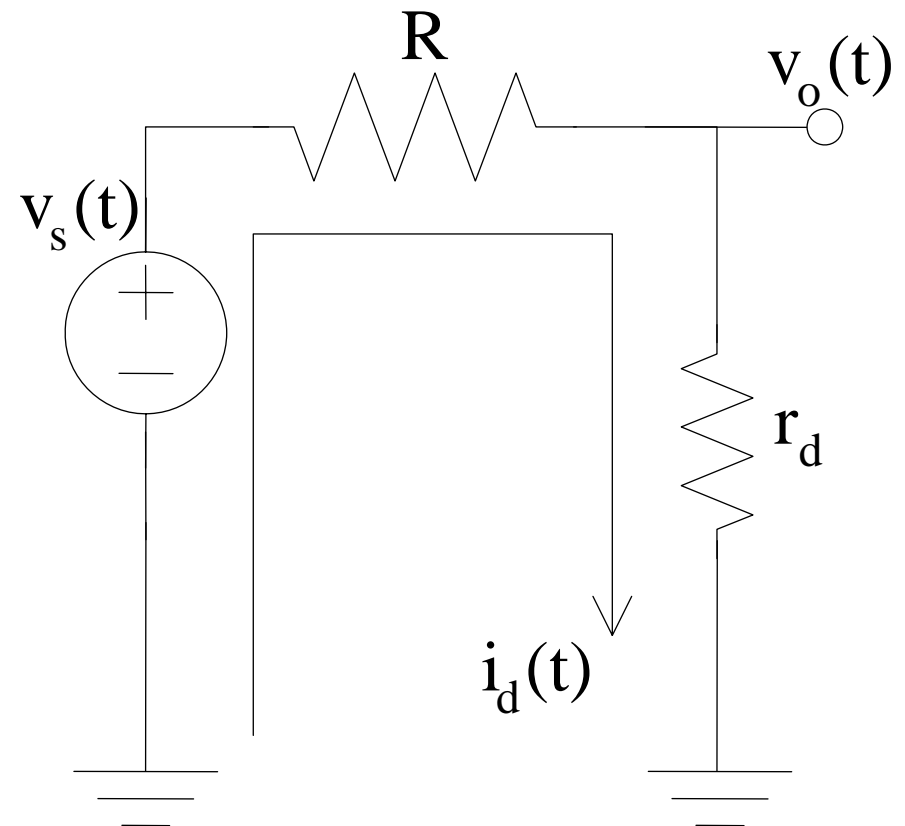
Complete AC Analysis

- Performing circuit analysis by first computing diode small signal resistance based on operating point:

$$r_d = \frac{n \cdot V_T}{I_D} = \frac{(1.1)(25mV)}{4.293mA} = 6.4\Omega$$

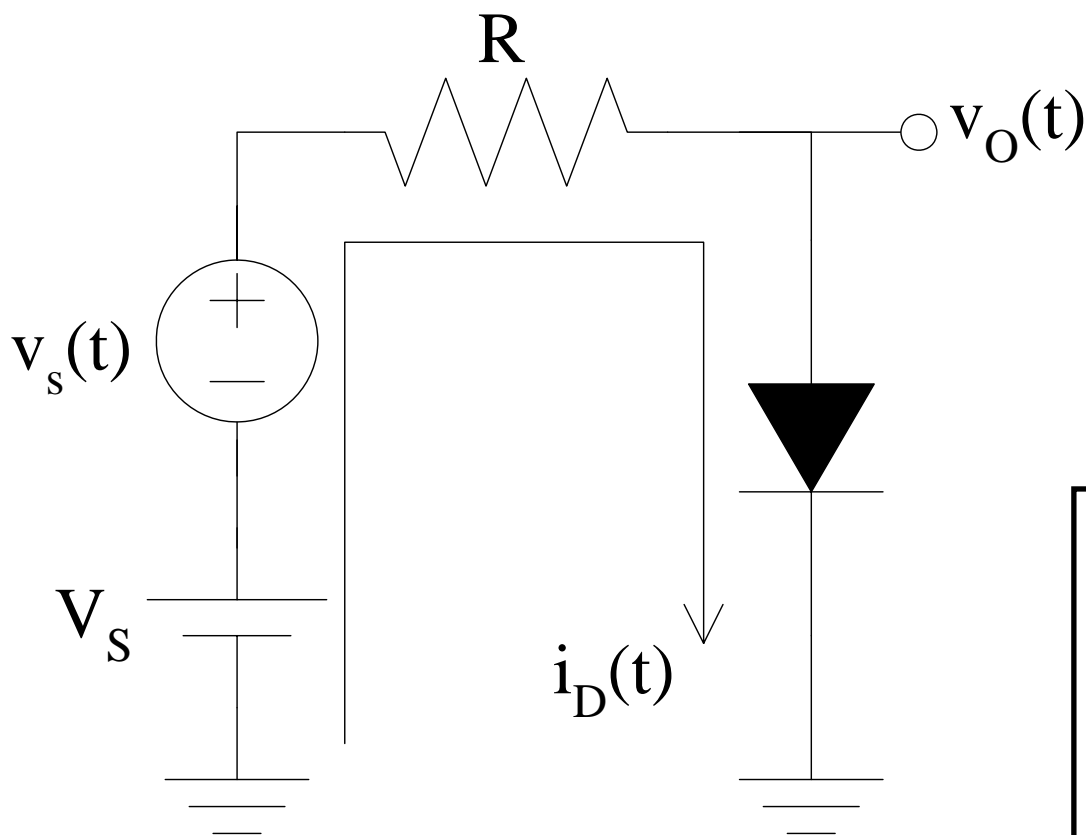
- Complete voltage divider circuit analysis:

$$\frac{v_o}{v_s} = \frac{r_d}{r_d + R} = \frac{6.4}{6.4 + 1k} = 6.36 \text{ mV/V}$$





Final Results- Linear Superposition



Total: $v_o(t) = V_O + v_o(t)$

DC: V_O

AC: $v_s(t) = V_p \sin(\omega t)$

$$\begin{aligned} v_o(t) &= V_O + v_o(t) \\ &= 0.7067 + \\ &\quad 0.0063 \cdot V_p \sin(\omega t) \end{aligned}$$



Small-Signal Analysis Technique Summary

- Tool for analyzing the behavior of circuits that contain nonlinear devices and have *small signal sources*
- Through linearization of the exponential model, we separate DC and AC analysis; linear superposition
- **Analysis procedure:**
 - Turn off AC sources, solve for DC operating point
 - Based on DC operating point parameters, solve for small signal-signal equivalent circuit model parameters
 - Construct small-signal equivalent circuit; short circuit voltage sources and open circuit current sources
 - Solve for AC parameters



Alternative Small-Signal Derivation Method of the text Book

$$i_D \approx I_S \exp\left(\frac{v_D}{n \cdot V_T}\right) \quad v_D \Rightarrow V_D + v_d$$
$$i_D \Rightarrow I_D + i_d$$

$$I_D + i_d = I_S \exp\left(\frac{V_D + v_d}{n \cdot V_T}\right) = I_S \exp\left(\frac{V_D}{n \cdot V_T}\right) \exp\left(\frac{v_d}{n \cdot V_T}\right)$$

$$I_D + i_d = I_D \exp\left(\frac{v_d}{n \cdot V_T}\right)$$



Condition for Small-Signal Derivation

$$I_D + i_d = I_D \left[1 + \frac{v_d}{n \cdot V_T} + \frac{\left(\frac{v_d}{n \cdot V_T} \right)^2}{2!} + \dots \right] \approx I_D \left[1 + \frac{v_d}{n \cdot V_T} \right]$$

$$i_d = v_d \frac{I_D}{n \cdot V_T} \Rightarrow \frac{v_d}{i_d} = \frac{n \cdot V_T}{I_D} = r_d$$

$$\frac{v_d}{n \cdot V_T} \ll 1$$

**The condition for small signal assumption
the applied AC signal:**

$$v_d \ll n V_T$$

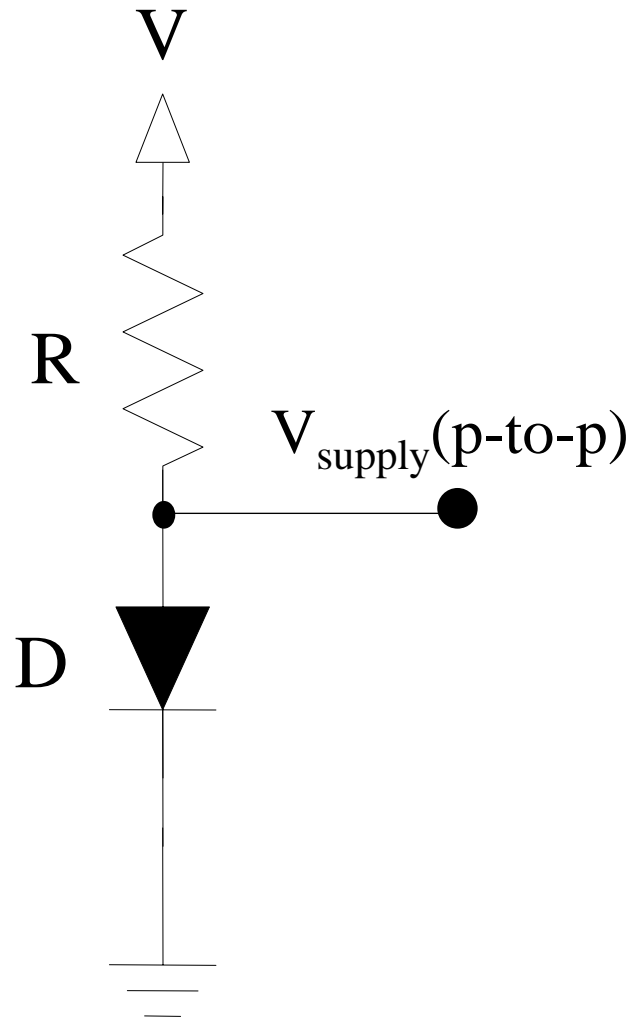


Small Signal Approximation

- Modeling diode as a resistor is an *approximation*
- Typically valid for signal amplitudes of order 10mV or less; this gets stretched to 25mV in some of S&S problems
- Although accurate, load line analysis and iterative analysis are not typically done when performing “hand” calculations of a diode circuit.
- DC voltage assumed to be 0.7V (CVDM) for purposes of determining I_D , and subsequently r_d



Example



- 1) Power supply: 10V with 60-Hz 1V peak amplitude fluctuation, also known as power supply ripple
- 2) $R=10\text{k}\Omega$
- 3) Diode: Assume 0.7V drop at 1mA of current and $n=2$

Find the peak-to-peak signal voltage across the diode due to power supply ripple.



Example (cont')

- Using DC information given, can compute I_D , the DC diode current:

$$I_D = \frac{10 - 0.7}{10k\Omega} = 0.93mA$$

- Using this value for I_D , can compute diode small signal resistance:

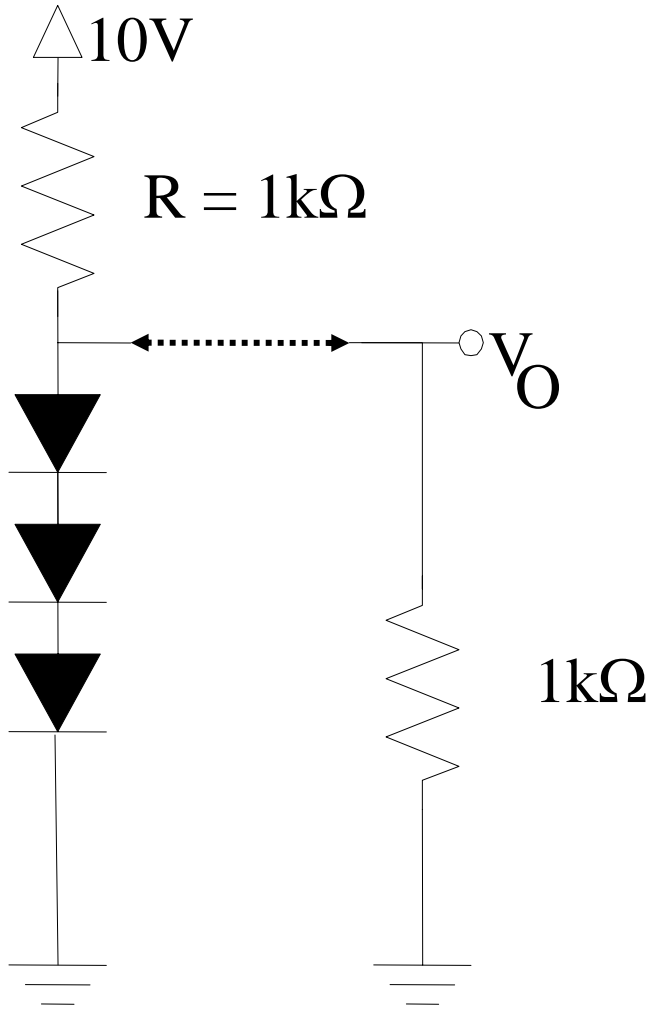
$$r_d = \frac{n \cdot V_T}{I_D} = \frac{(2)(25mV)}{0.93mA} = 53.8\Omega$$

- Peak-to-peak signal voltage across diode found using voltage divider circuit analysis:

$$v_d(\text{peak-to-peak}) = 2V \frac{r_d}{R_D + r_d} = 2V \frac{53.8}{10k\Omega + 53.8} = 10.7mV$$



Example



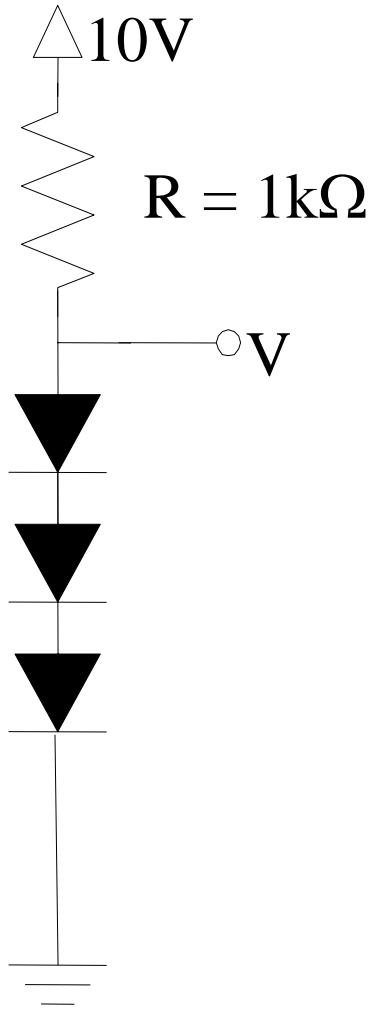
Consider circuit with 3 diodes in series with a resistor and power supply.

Calculate the percentage change in the voltage across the diodes caused by connecting a $1\text{k}\Omega$ resistor.

All diodes have $n=2$ and can assume CVD model for DC analysis.



Compute Diode Small Signal Resistance



- Start assuming resistor not attached; $V_O = 2.1V$ ($3 \times 0.7V$).
- Nominal current through string

$$I = \frac{10 - 2.1}{1k\Omega} = 7.9mA$$

- Diode small signal resistance

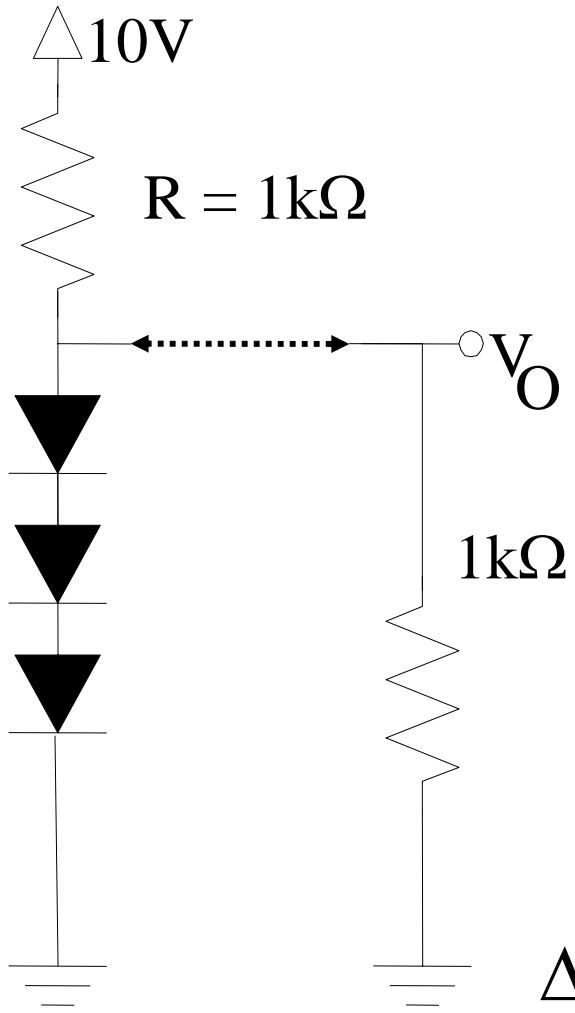
$$r_D = \frac{2 \times 0.25mV}{7.9mA} = 6.3\Omega$$

- Total resistance

$$r = 3r_d = 18.9\Omega$$



Compute Impact of Attaching Load



- Hook up load resistor and estimate how much current will be drawn by the load; since DC voltage drop across 3 diodes is 2.1 V, can assume

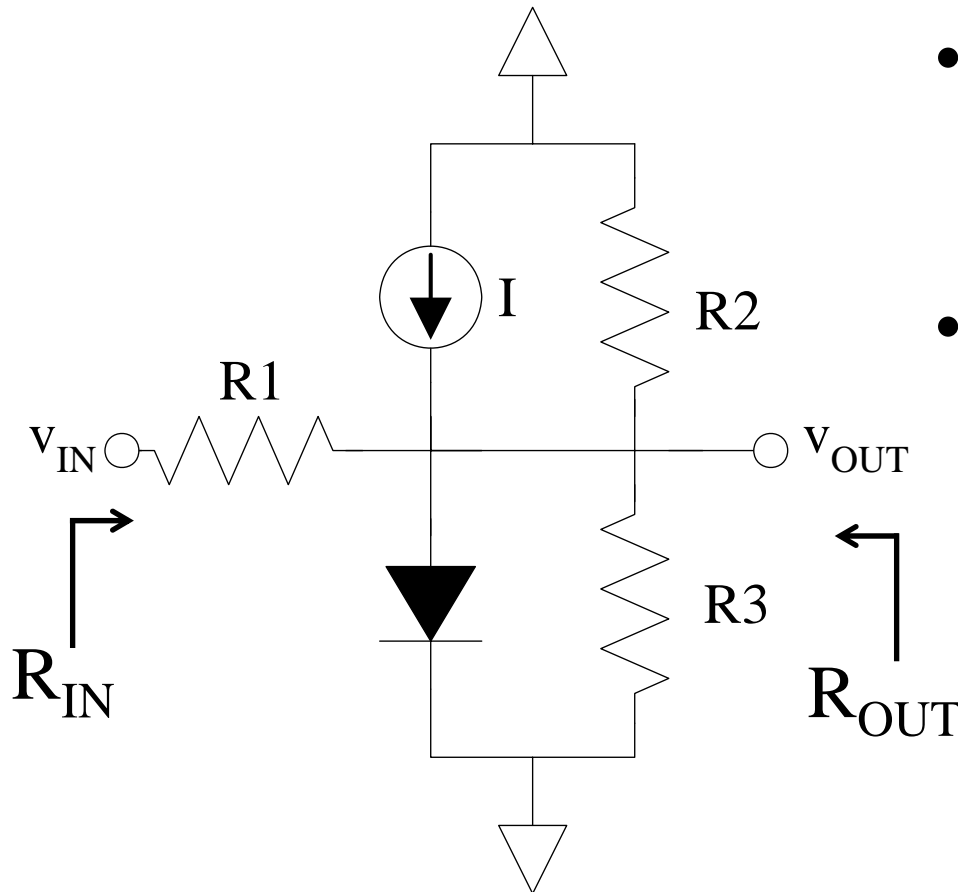
$$I_{load} \approx \frac{2.1V}{1k\Omega} = 2.1mA$$

- Result is a reduction in diode current of ~ 2.1 mA; can use this to calculate reduction in v_o :

$$\Delta v_o = -2.1 \times r = -2.1 \times 18.9 = -39.7mV$$



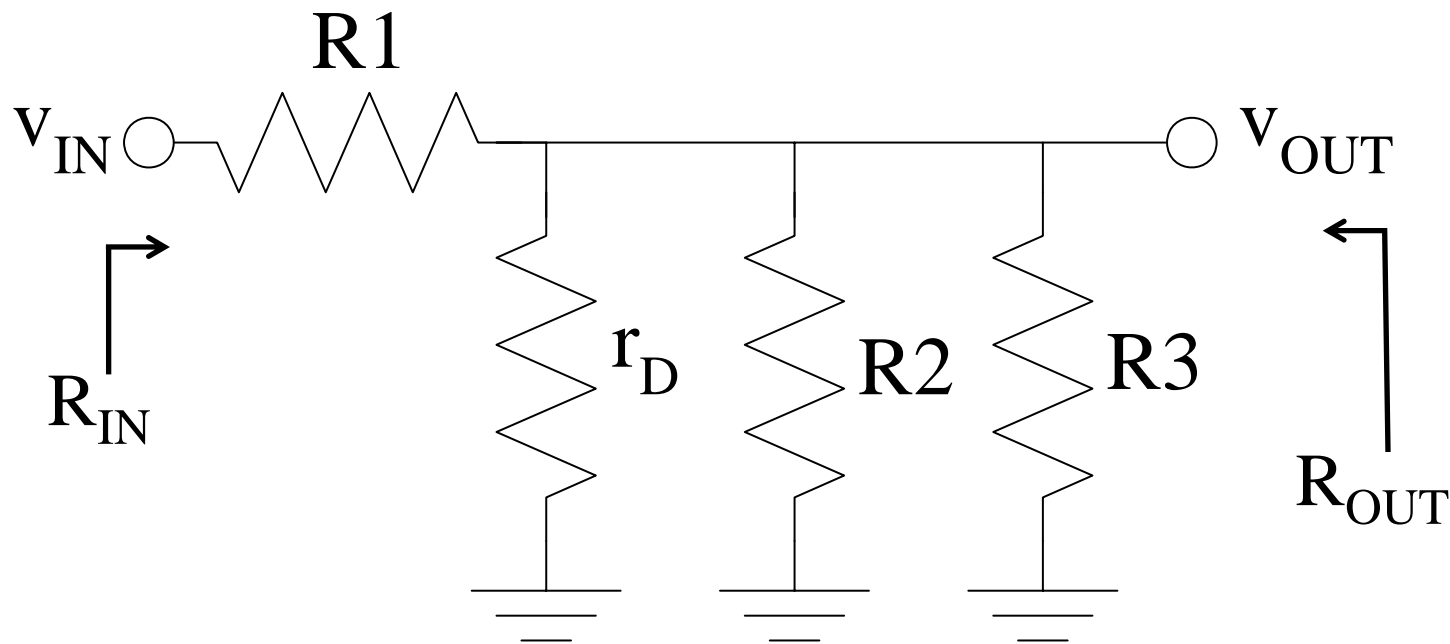
Input/Output Signal Resistance



- Consider following circuit with DC voltage and current sources
- Compute R_{IN} & R_{OUT} the small signal resistance seen at the input and output, respectively



Draw Small Signal Equivalent Circuit

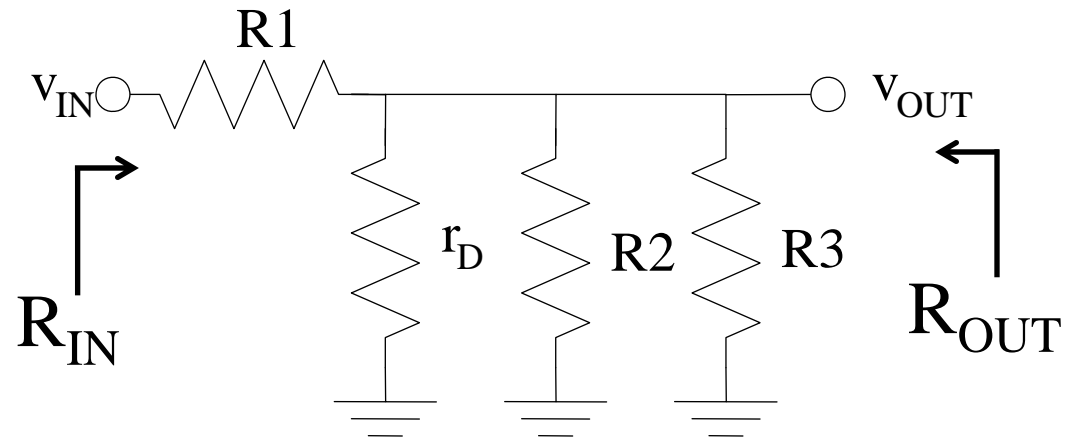


Note: In AC/small signal analysis batteries (DC Supply voltages) are short circuited and current sources are open circuited



Compute Input/Output Signal Resistance

- Find R_{IN} by inspection
- For R_{OUT} , use method #2 (discussed in the introduction to amplifiers slides)
- Ground v_{IN} in the small-signal circuit
- Now, find R_{OUT} by inspection:



$$R_{IN} = R_1 + r_D \parallel R_2 \parallel R_3$$

$$R_{OUT} = R_1 \parallel r_D \parallel R_2 \parallel R_3$$